

# **MODELING THE EFFECT OF AEROBIC BIODEGRADATION ON VAPOR INTRUSION**

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# Objectives

Apply Abreu and Johnson 3D model to:

- Visualize predicted concentration profiles around buildings for biodegradable chemicals
- Evaluate how aerobic biodegradation affects the attenuation factor  $\alpha$  as a function of:
  - Vapor source concentration
  - Vapor source depth
  - Lateral distance from buildings
  - Biodegradation rates
  - Cracks location
  - Building construction

$$\alpha = C^{\text{indoor}}/C^{\text{source}}$$



# The Abreu and Johnson 3D Model

- The numerical code couples equations for the soil gas pressure field and air flow field with the multi-species contaminant transport and reaction equation
- Solved by finite differences method
- Time-varying building and atmospheric pressurization
- Multi-component systems (e.g., O<sub>2</sub>, hydrocarbons)
- User-defined kinetics
- Variable building construction (basements, slabs, varying crack sizes and crack locations)
- Variable source characteristics (location, strength)
- Heterogeneous subsurface settings

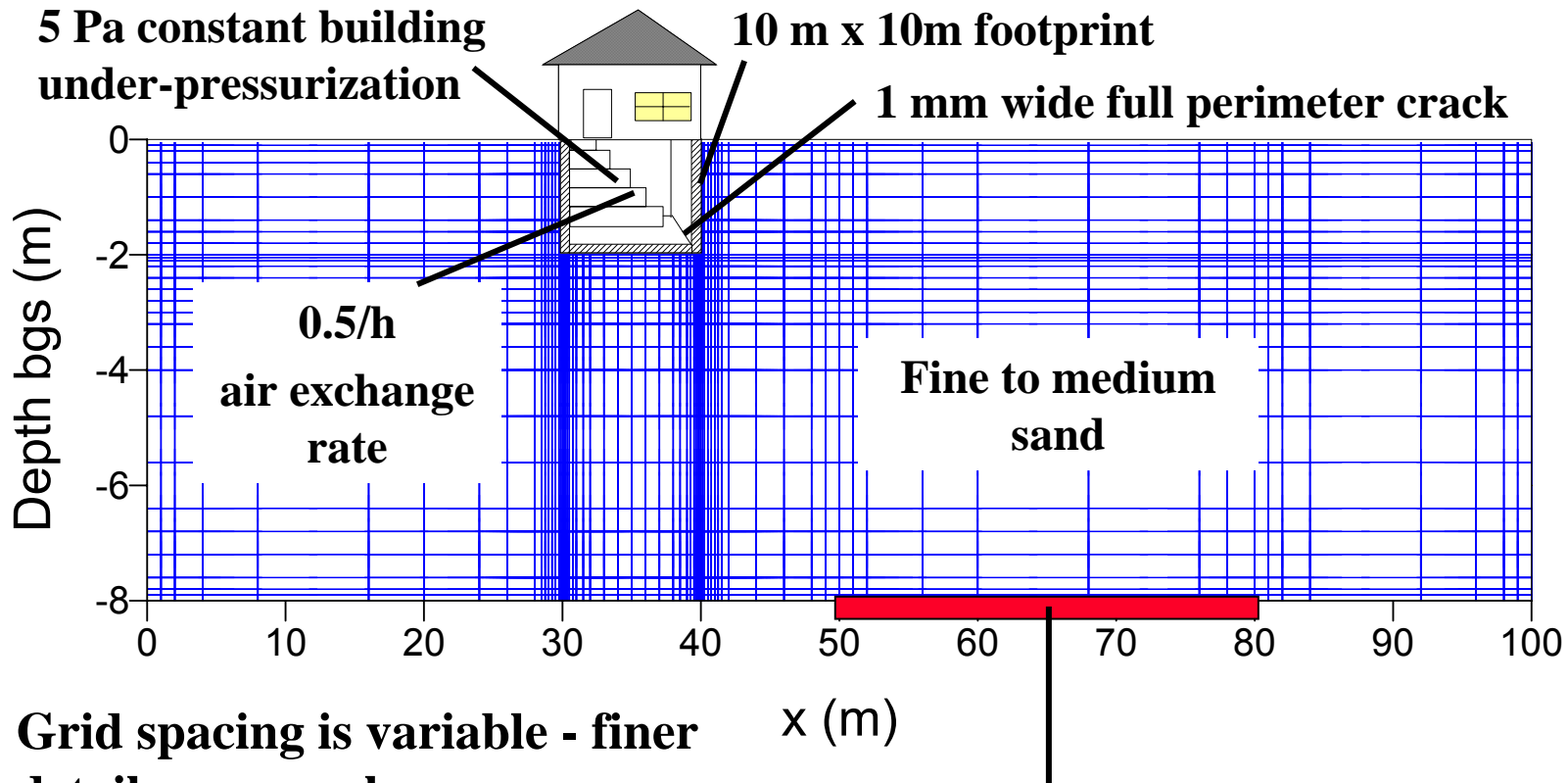
$$\frac{\partial P}{\partial t} - \left( \frac{\bar{P}}{\phi_g \mu_g} \right) \cdot \vec{\nabla} \cdot (\mathbf{K}_g \cdot \vec{\nabla} P) = 0 \quad \vec{q}_g = \frac{K_g}{\mu_g} (\vec{\nabla} p)$$

$$a_i \cdot \frac{\partial C_{ig}}{\partial t} = -\vec{\nabla} \cdot (C_{ig} \cdot \vec{q}_g) - \vec{\nabla} \cdot \left( \frac{C_{ig}}{H_i} \cdot \vec{q}_w \right) + \vec{\nabla} \cdot (D_i \cdot \vec{\nabla} C_{ig}) - R_i$$

$$Q_{ck} = \left( -\frac{w_{ck}^3}{12\mu_g \cdot d_{ck}} \right) [p - p^{\text{indoor}}] = w_{ck} \left( \frac{K_g}{\mu_g} \right) \frac{\partial p}{\partial z}$$



# Model Inputs



Grid spacing is variable - finer detail near cracks, source boundaries, and domain boundaries

# Model Predicted Pressure Fields

Basement scenarios

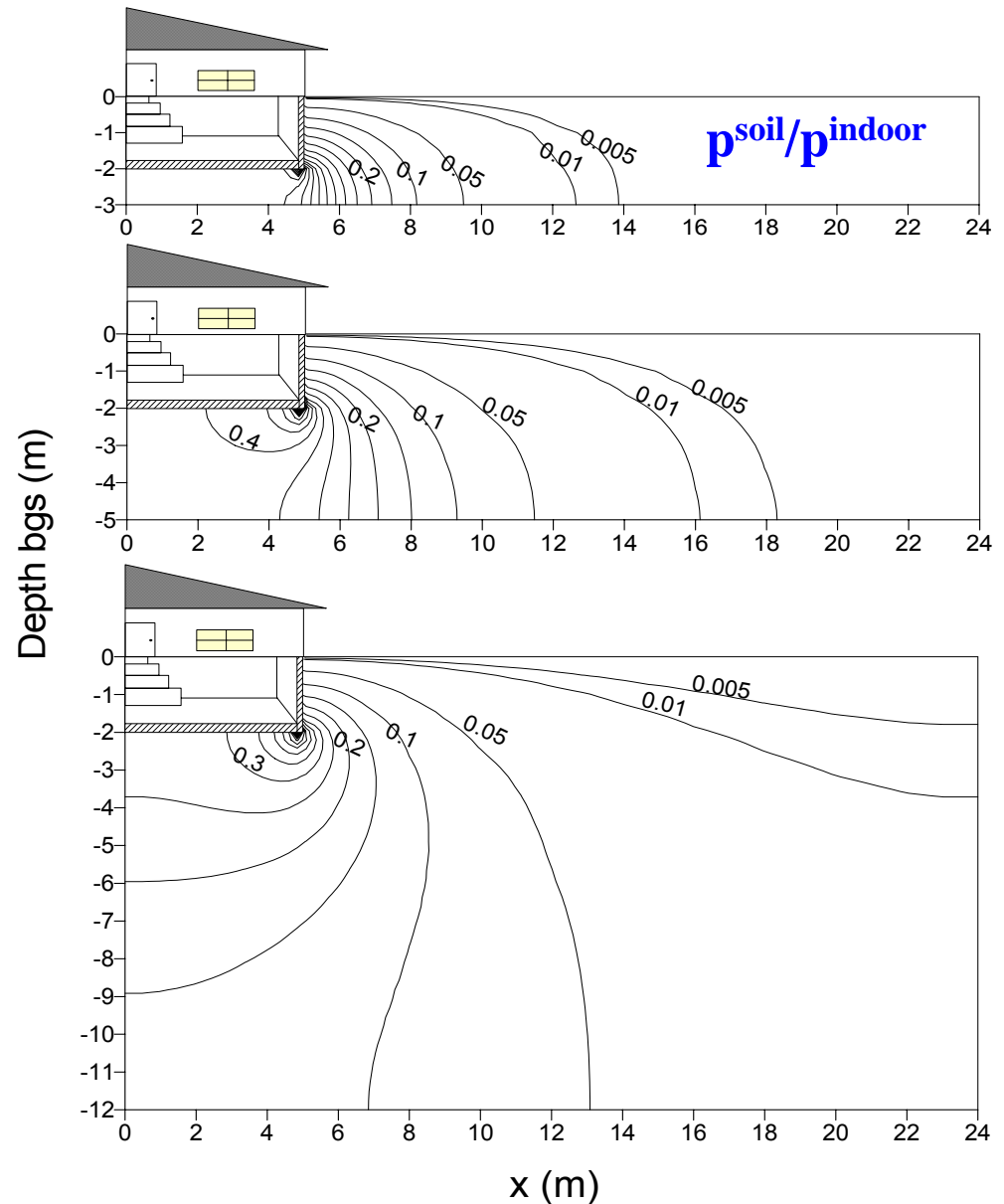
Perimeter crack

Homogeneous soil

Cross-section through  
plane of symmetry

$$p^{\text{soil}} = P_{\text{atm}} - p^{\text{soil}}$$

$$p^{\text{indoor}} = P_{\text{atm}} - p^{\text{indoor}}$$



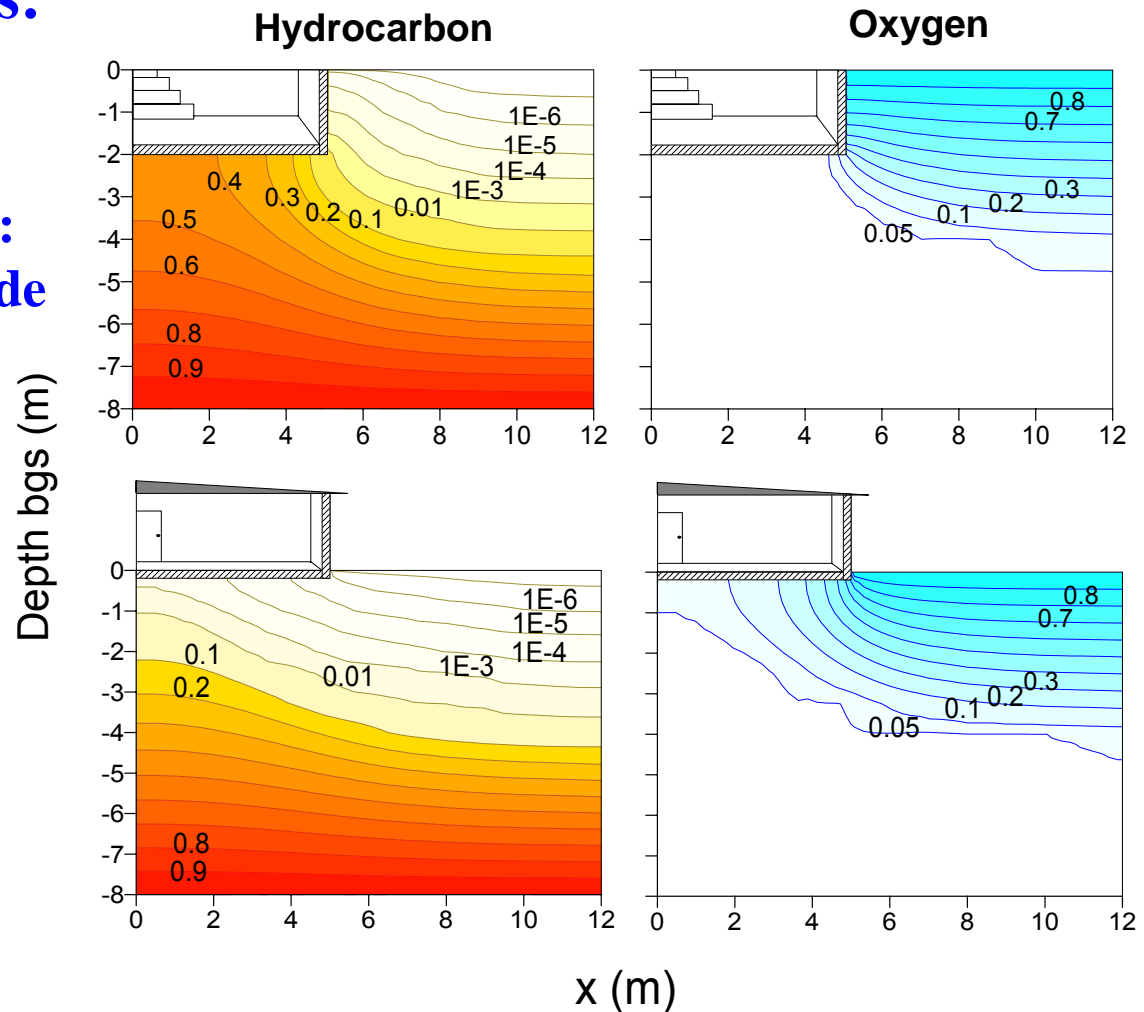
# Effect of Aerobic Biodegradation

## Presentation of results:

Concentration profiles on vertical cross-sections through center of building: Basement and slab-on-grade

Hydrocarbon conc. contour plots normalized to the source zone vapor concentration at the lower boundary

Oxygen conc. contour plots normalized to the atmospheric conc. at the ground surface



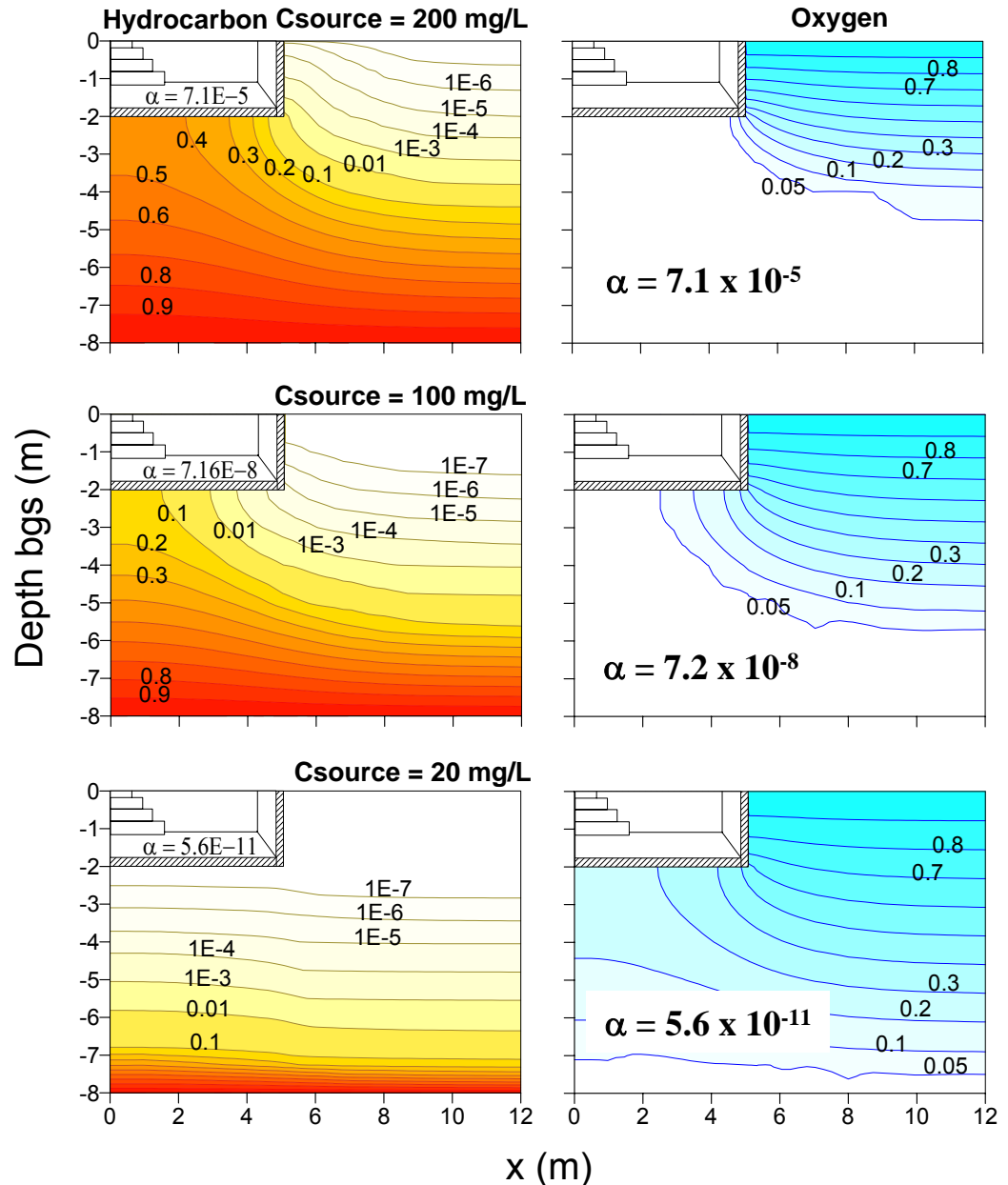
# Effect of Source Concentration

[Basement Scenario]

$[\lambda = 0.18 \text{ h}^{-1}]$

Results suggest that there may be source vapor concentrations that are of little concern if soil gas beneath the foundation is well-oxygenated

(e.g., low concentration dissolved petroleum groundwater plume sources)

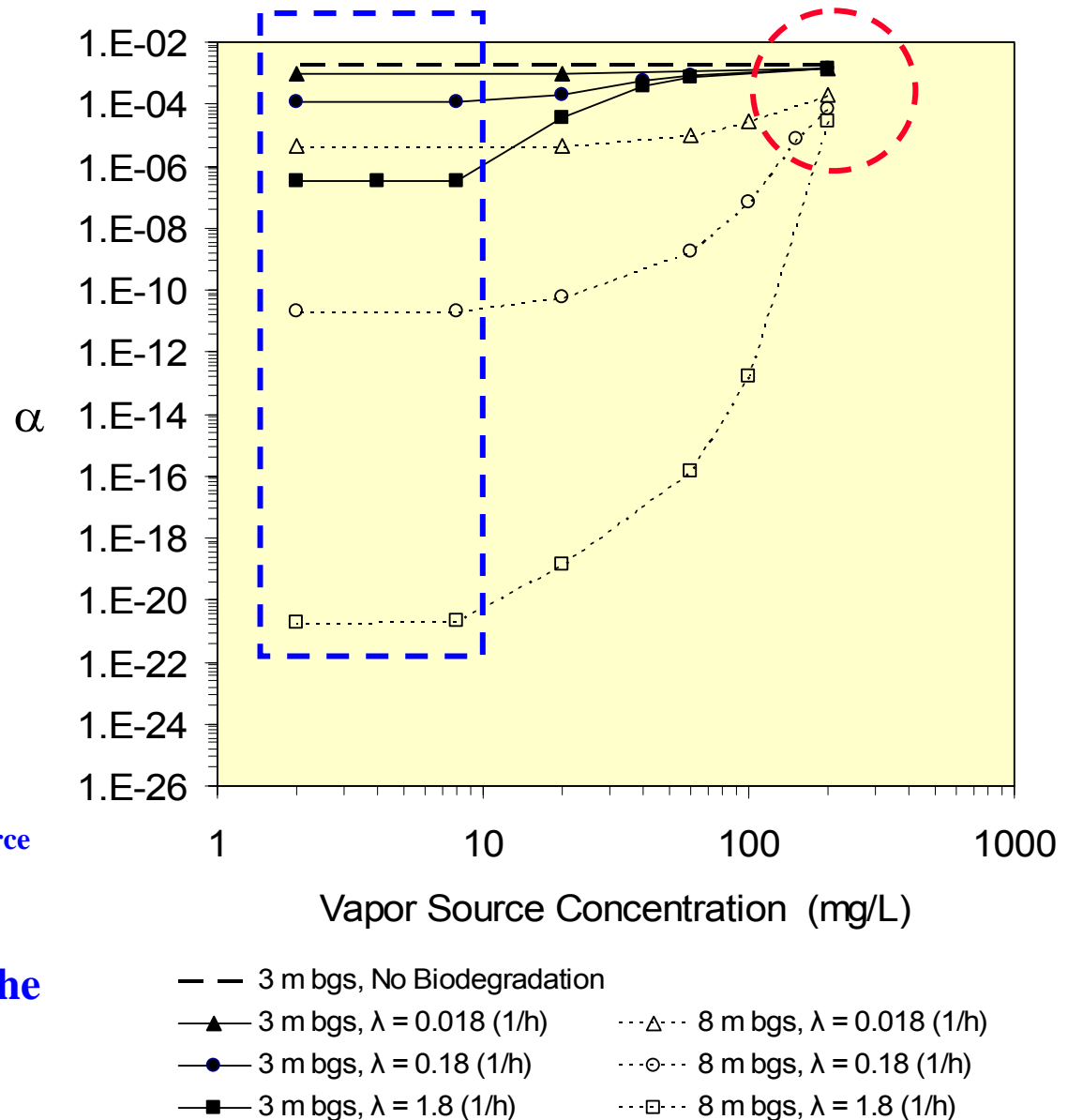


# Effect of Source Conc. on $\alpha$

[Basement Scenario]

At high concentrations, the effect of biodegradation on  $\alpha$  is minimal due to oxygen depletion beneath and near foundation

At low concentrations,  $\alpha$  becomes independent of  $C_{\text{source}}$  because of the first-order kinetics and oxygen rich conditions everywhere, and the effect of biodegradation is more pronounced



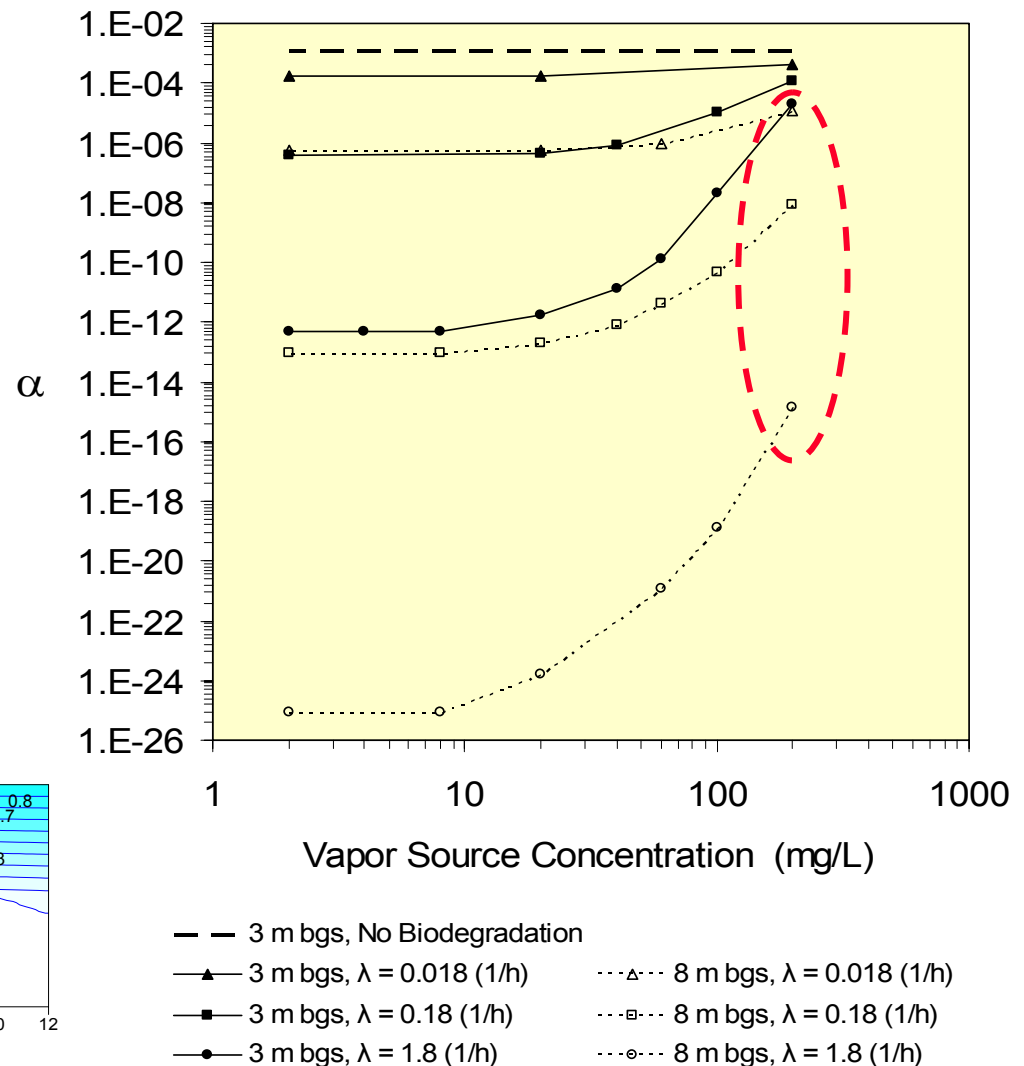
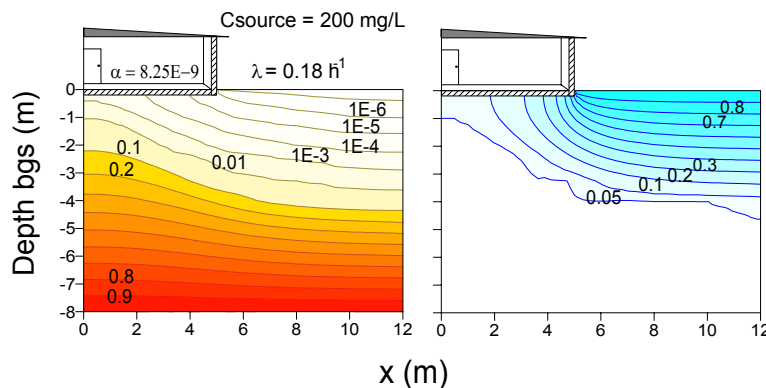


# Effect of Source Conc. on $\alpha$

[Slab-on-grade Scenario]

Similar trends as of  
basement scenario  
but  $\alpha$  values are lower and  
it is more sensitive to  $\lambda$

For high vapor source  
concentrations at 8 m bgs  
oxygen penetrates fully  
beneath the slab and the  
effect of biodegradation on  
 $\alpha$  is significant



# Effect of Depth

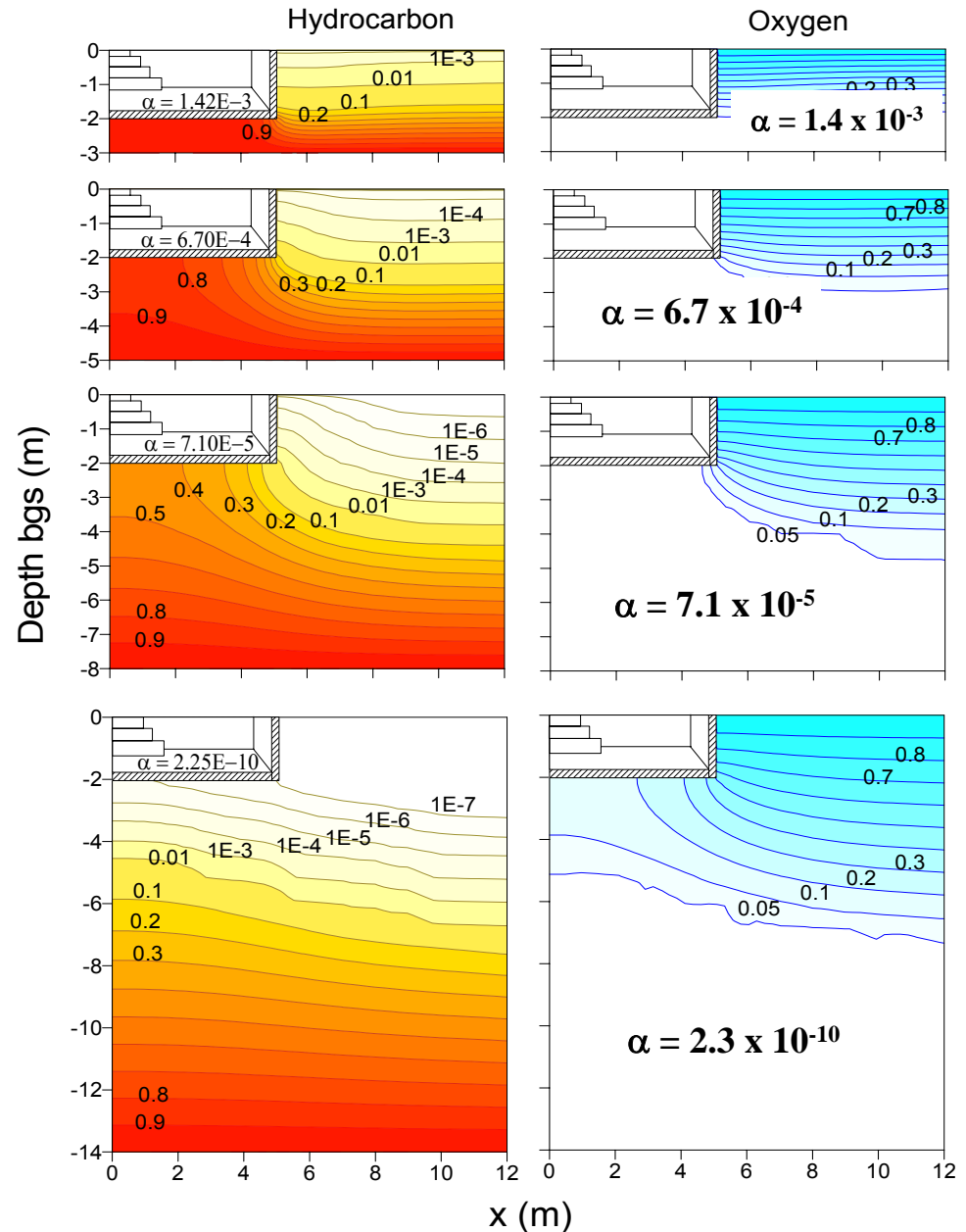
[Basement Scenario]

[C<sub>source</sub> = 200 mg/L ]

[ $\lambda = 0.18 \text{ h}^{-1}$ ]

Results suggest that, for a given source vapor concentration, there may be a critical depth beyond which vapor migration is of little concern

This depth will be a function of concentration and degradation rate at a minimum.



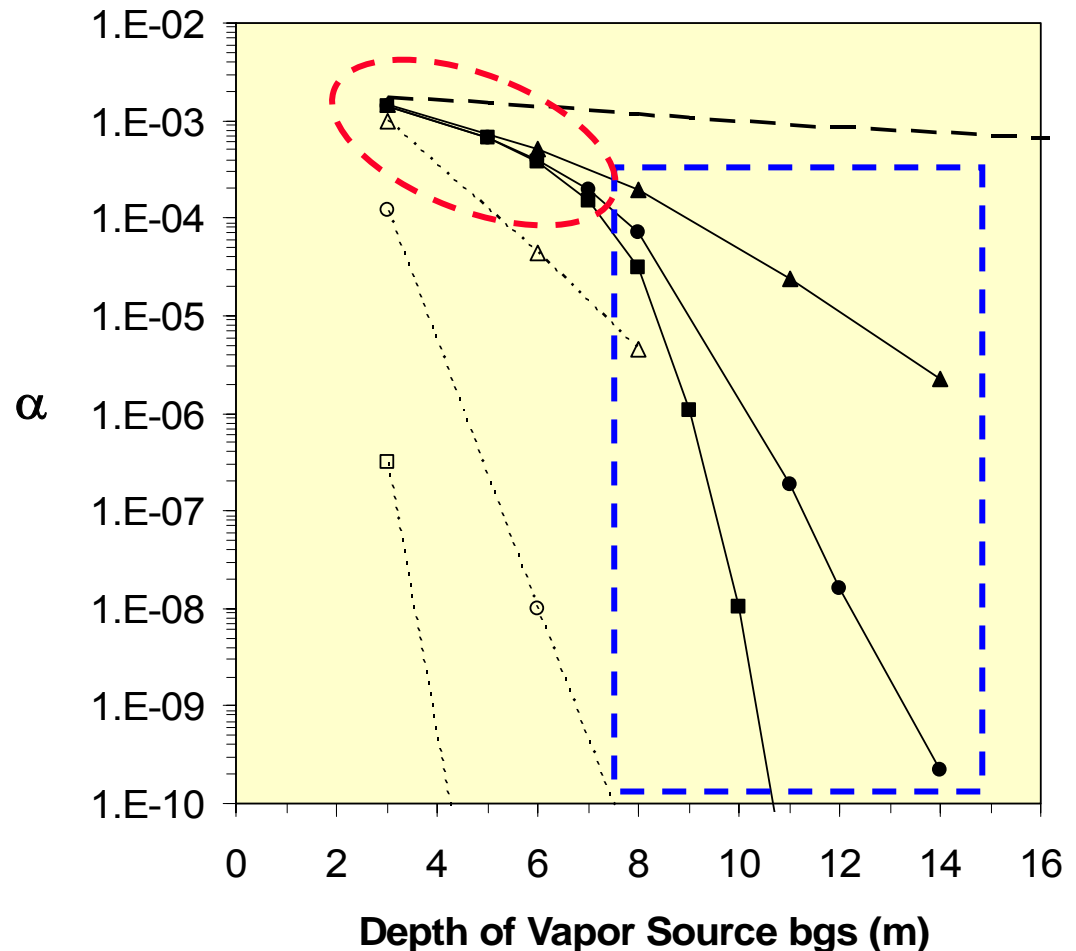
# Effect of Depth on $\alpha$

[Basement Scenario]

Combinations of source strength, source depth, and first-order biodegradation rate ( $\lambda$ )

High concentration cases show lower sensitivity to  $\lambda$  changes and depths for depths less than 8 m

Increasing sensitivity in  $\alpha$  to depth and  $\lambda$  occurs as the depth increases and as the source vapor concentration decreases

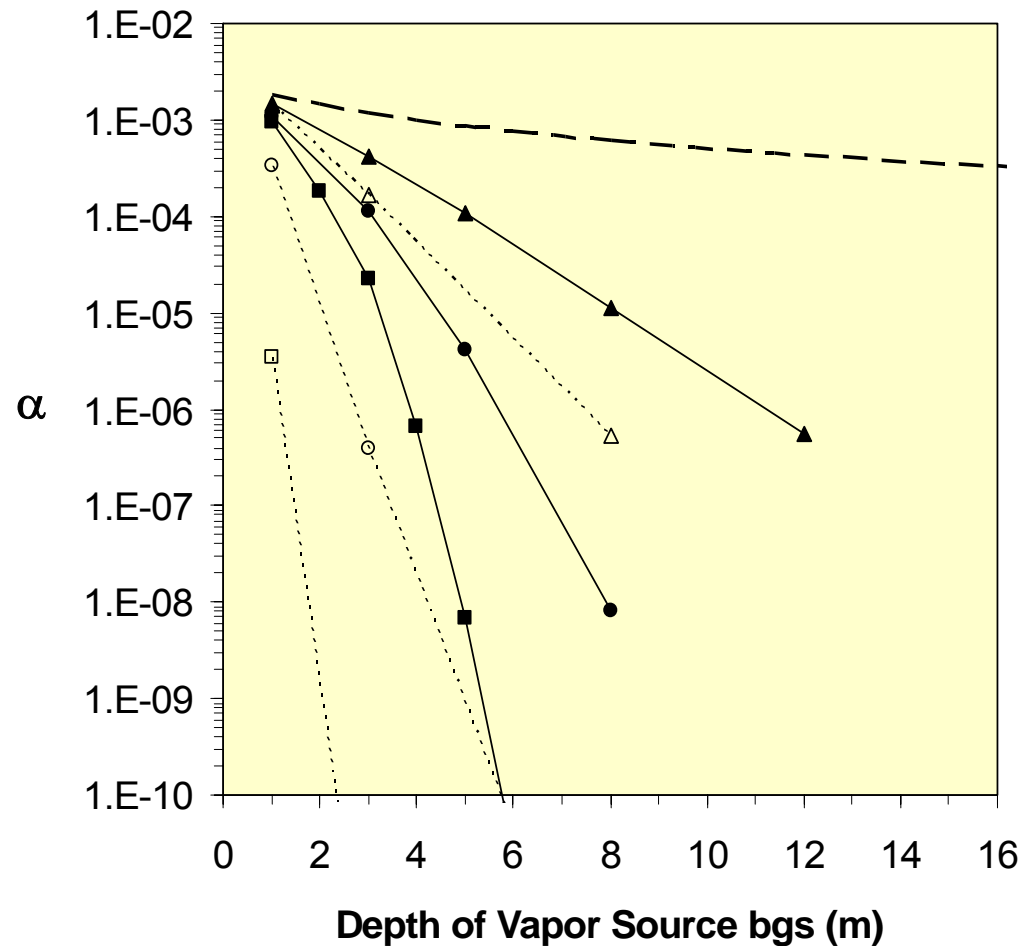
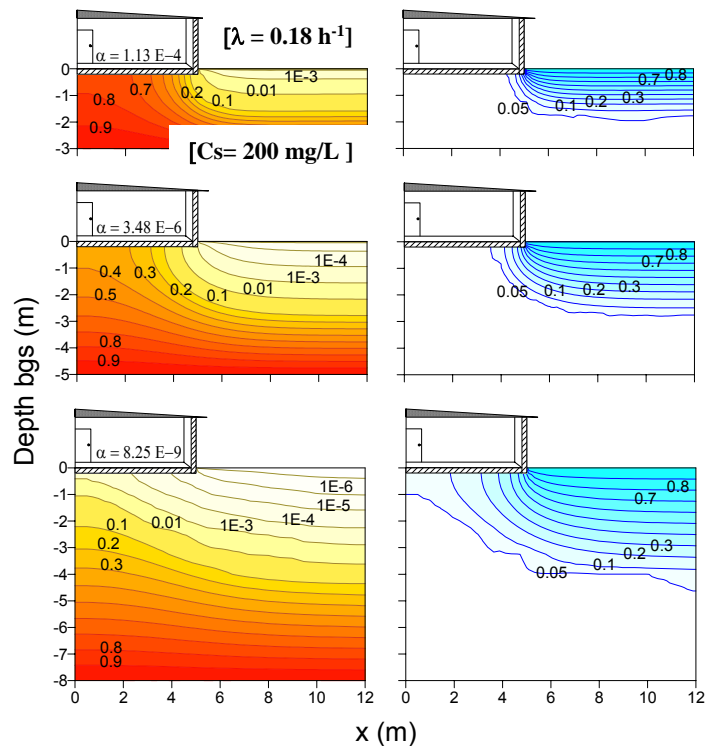


- — No Biodegradation
- △--- 2 mg/L,  $\lambda = 0.018$  (1/h)
- 2 mg/L,  $\lambda = 0.18$  (1/h)
- 2 mg/L,  $\lambda = 1.8$  (1/h)
- ▲— 200 mg/L,  $\lambda = 0.018$  (1/h)
- 200 mg/L,  $\lambda = 0.18$  (1/h)
- 200 mg/L,  $\lambda = 1.8$  (1/h)

# Effect of Depth on $\alpha$

[Slab-on-Grade Scenario]

Lower  $\alpha$  values and more  
sensitivity to depth than the  
basement scenario



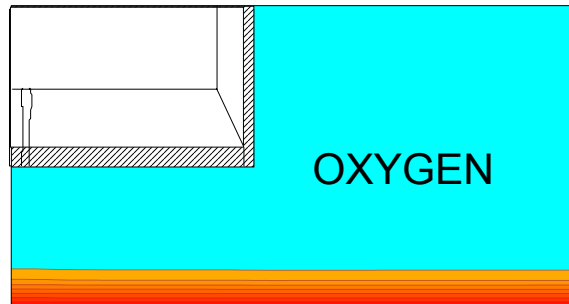
- — No Biodegradation
- △--- 2 mg/L,  $\lambda = 0.018$  (1/h)
- 2 mg/L,  $\lambda = 0.18$  (1/h)
- 2 mg/L,  $\lambda = 1.8$  (1/h)
- ▲— 200 mg/L,  $\lambda = 0.018$  (1/h)
- 200 mg/L,  $\lambda = 0.18$  (1/h)
- 200 mg/L,  $\lambda = 1.8$  (1/h)

# Effect of crack location on $\alpha$

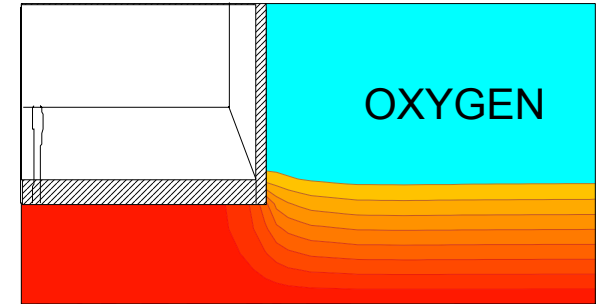
## Not sensitive if

- Oxygen penetrates deep into the subsurface and fully beneath slab or
- Oxygen does not penetrate beneath the slab

Low conc. sources  
Deep sources



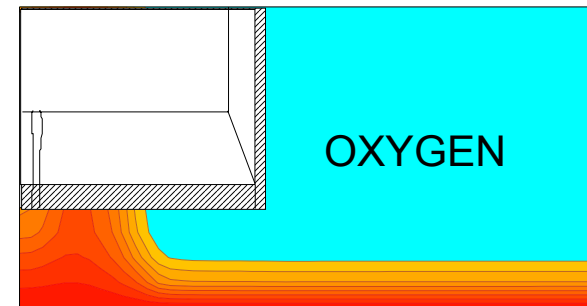
High conc. sources  
Shallow sources



## May be sensitive if

- Oxygen penetrates only partially beneath the slab

Transition between:  
high-low source conc.  
shallow-deep sources



## The sensitivity is a function of:

- Source depth
- Source concentration
- Foundation type
- Degradation rate

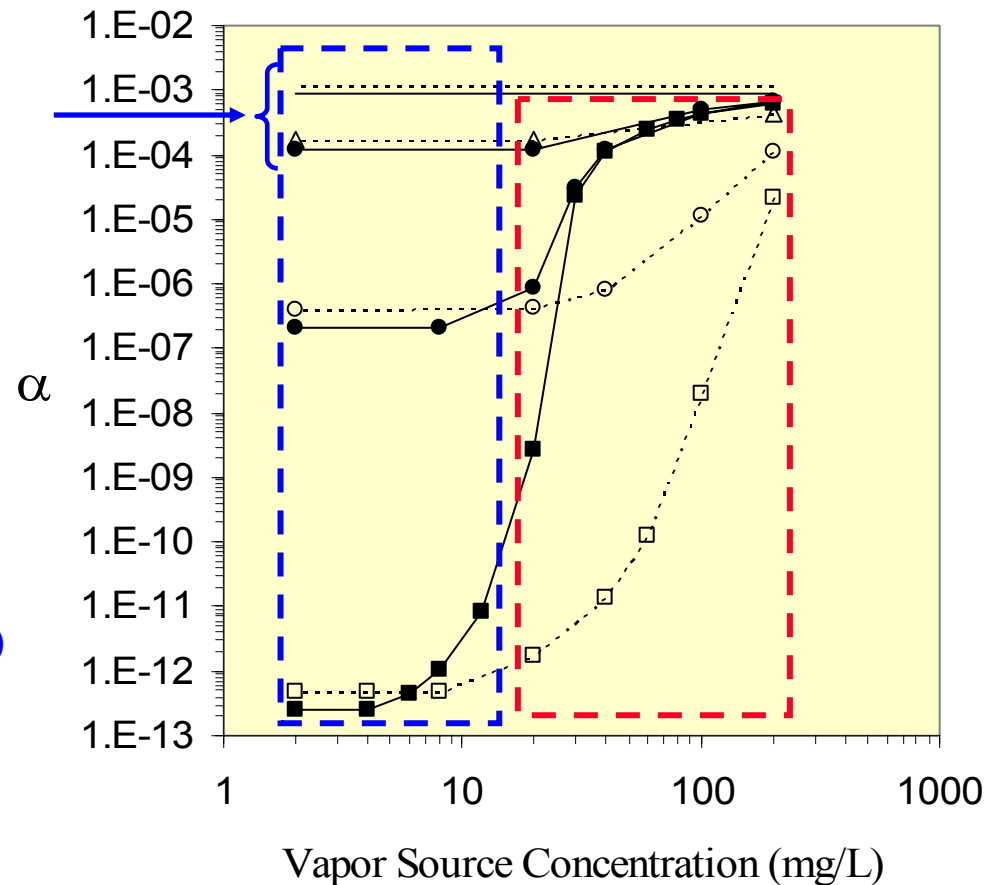
# Effect of crack location on $\alpha$ as func. of conc.

Slab-on-Grade Scenario,  
Source at 3m bgs

Not significant for non-degradation  
or low  $\lambda$  cases (at any concentration)

Not significant for conc. <20 mg/L  
(for any  $\lambda$  case)

Significant for medium and  
high degradation rate scenarios  
in the concentration range of  
20-200 mg/L



- Crack in the perimeter, No reactions
- Crack in the center, No reactions
- △--- Crack in the perimeter,  $\lambda = 0.018$  (1/h)
- Crack in the perimeter,  $\lambda = 0.18$  (1/h)
- Crack in the perimeter,  $\lambda = 1.8$  (1/h)
- Crack in the center,  $\lambda = 0.018$  (1/h)
- Crack in the center,  $\lambda = 0.18$  (1/h)
- Crack in the center,  $\lambda = 1.8$  (1/h)

# Effect of crack location on $\alpha$ as func. of depth

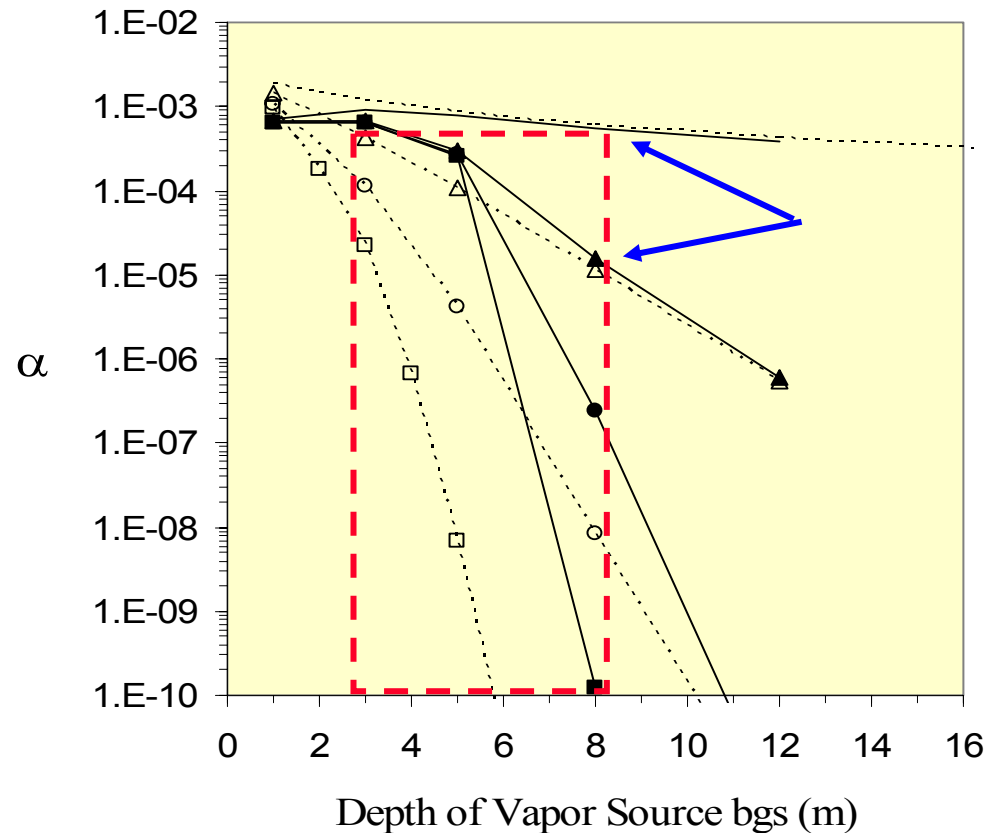
Slab-on-Grade Scenario

High source conc. = 200 mg/L

Not significant for non-degradation or low  $\lambda$  cases (at any depth)

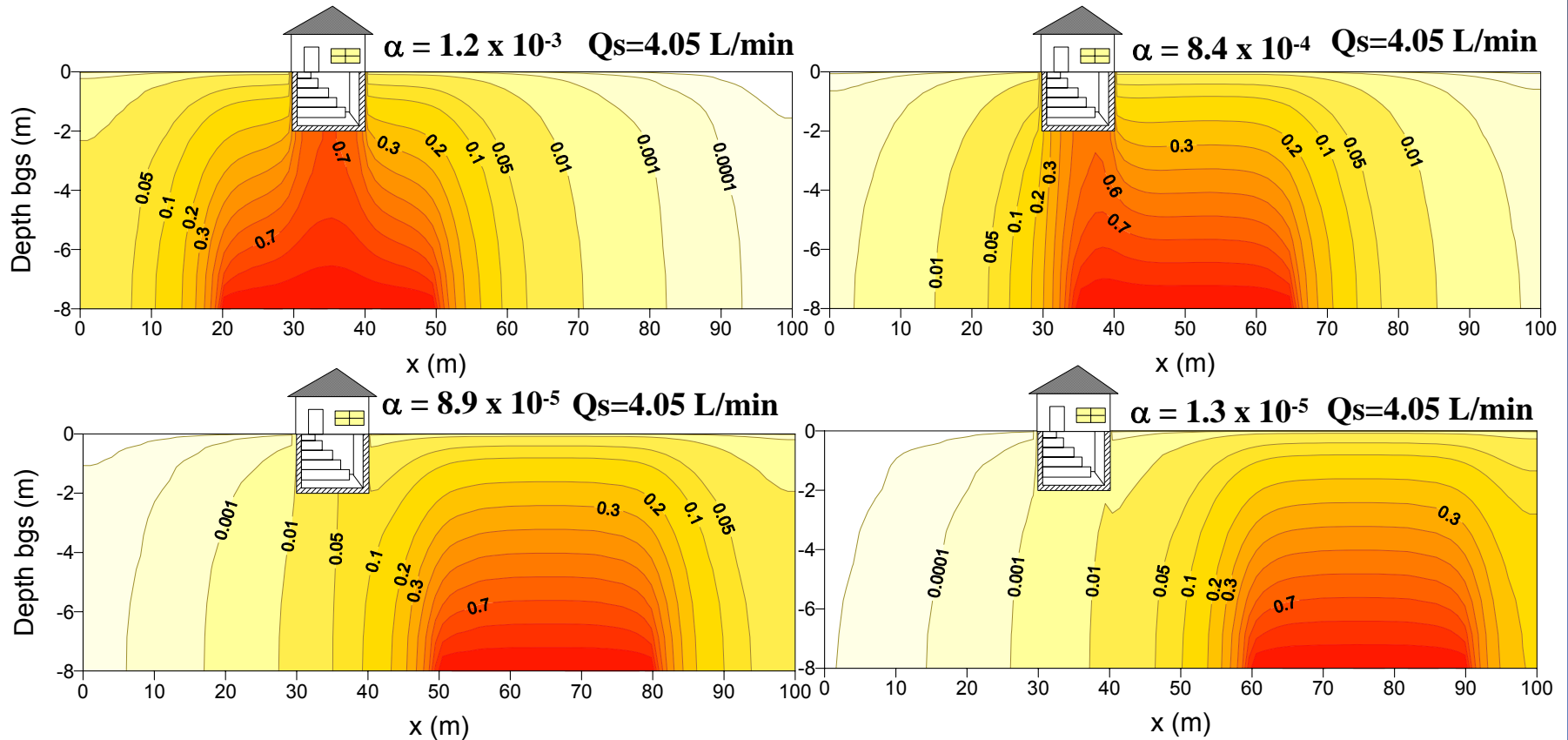
Not significant for depths >9 m bgs (for any  $\lambda$  case)

Significant for medium and high degradation rate scenarios in the depth range of 3-8 m bgs



# Changes in $\alpha$ with Source Position

[No degradation scenario]





# Changes in $\alpha$ with Source Position

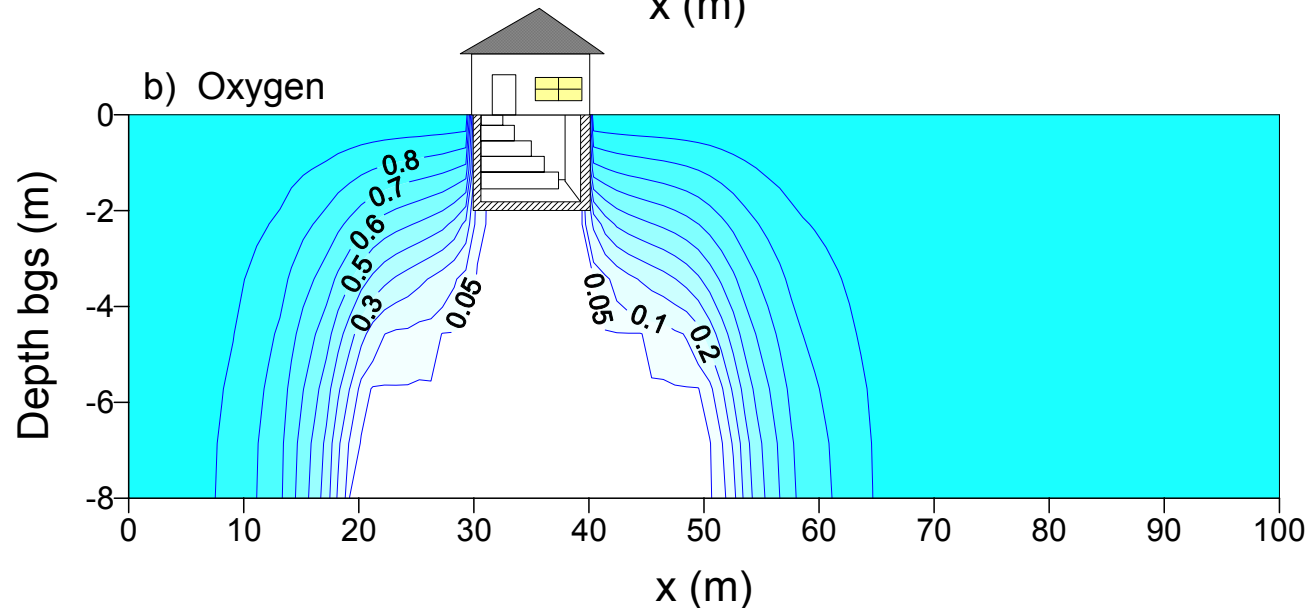
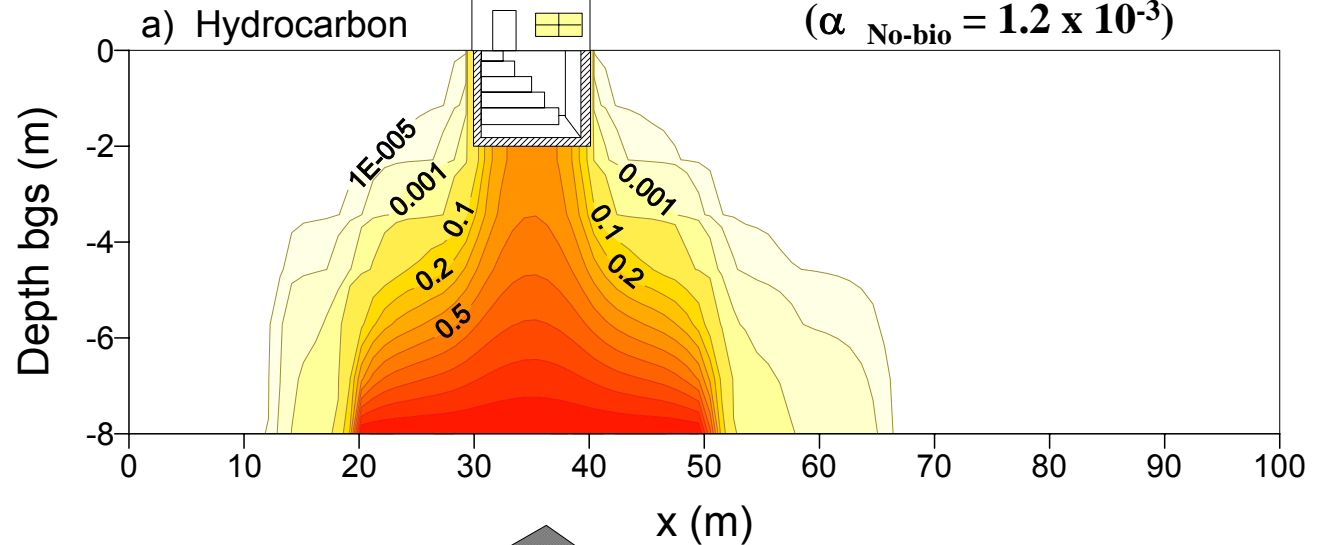
[Biodegradation,  
Basement Scenarios,  
 $C_{\text{source}} = 200 \text{ mg/L}$ ]

$$\lambda = 0.18 \text{ h}^{-1}$$

$$Q_s = 4.05 \text{ L/min}$$

$$\alpha_{\text{bio}} = 6.8 \times 10^{-5}$$

$$(\alpha_{\text{No-bio}} = 1.2 \times 10^{-3})$$



# Changes in $\alpha$ with Source Position

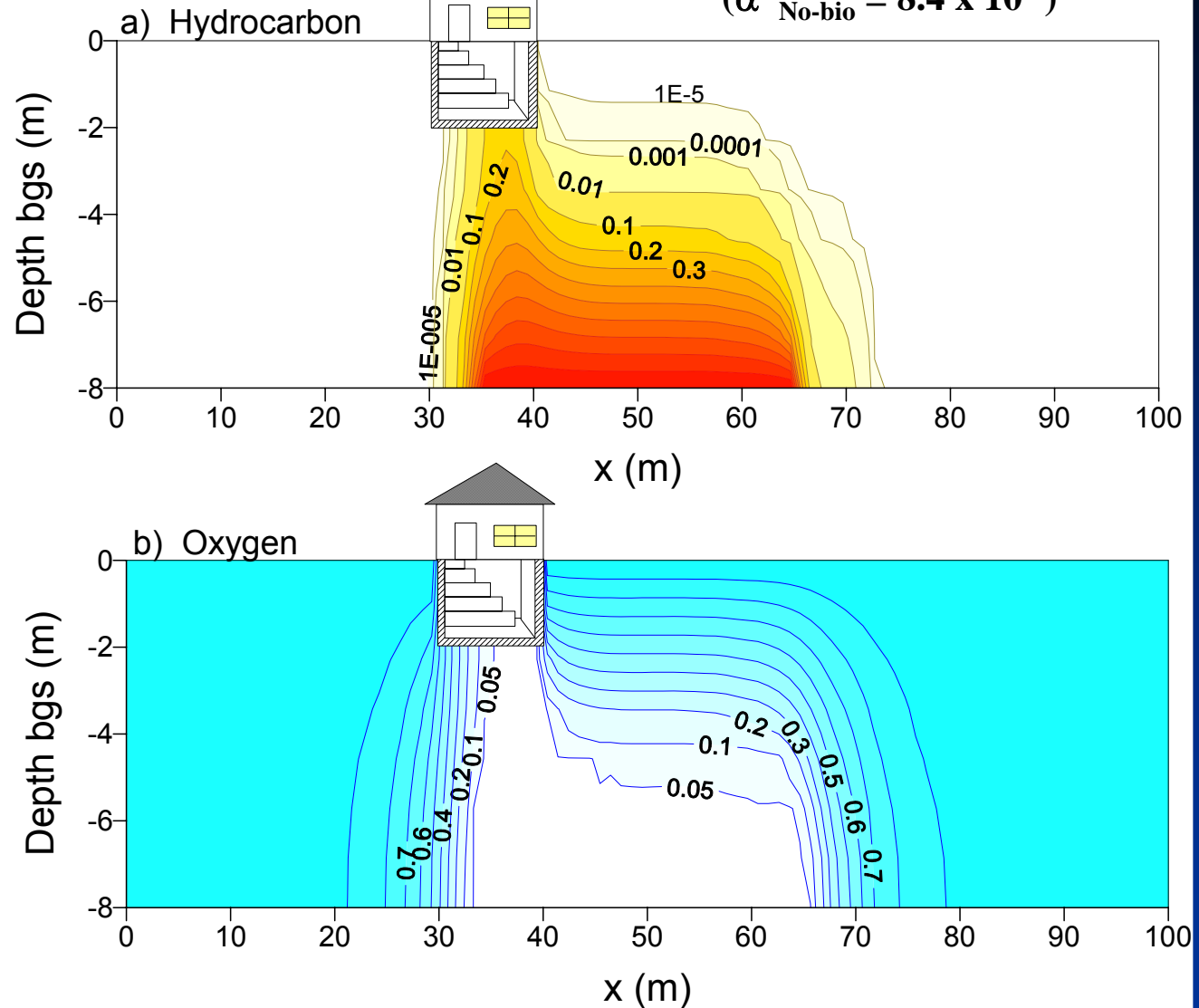
[Biodegradation,  
Basement Scenarios,  
 $C_{\text{source}} = 200 \text{ mg/L}$ ]

$$\lambda = 0.18 \text{ h}^{-1}$$

$$Q_s = 4.05 \text{ L/min}$$

$$\alpha_{\text{bio}} = 5.0 \times 10^{-6}$$

$$(\alpha_{\text{No-bio}} = 8.4 \times 10^{-4})$$



# Changes in $\alpha$ with Source Position

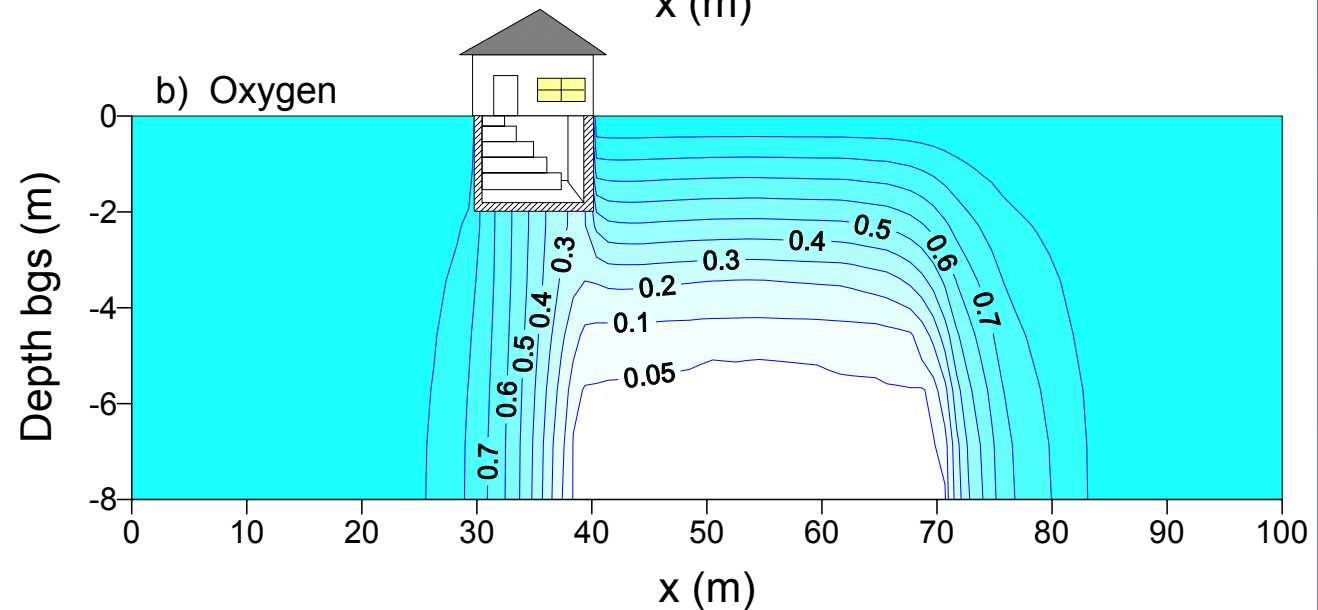
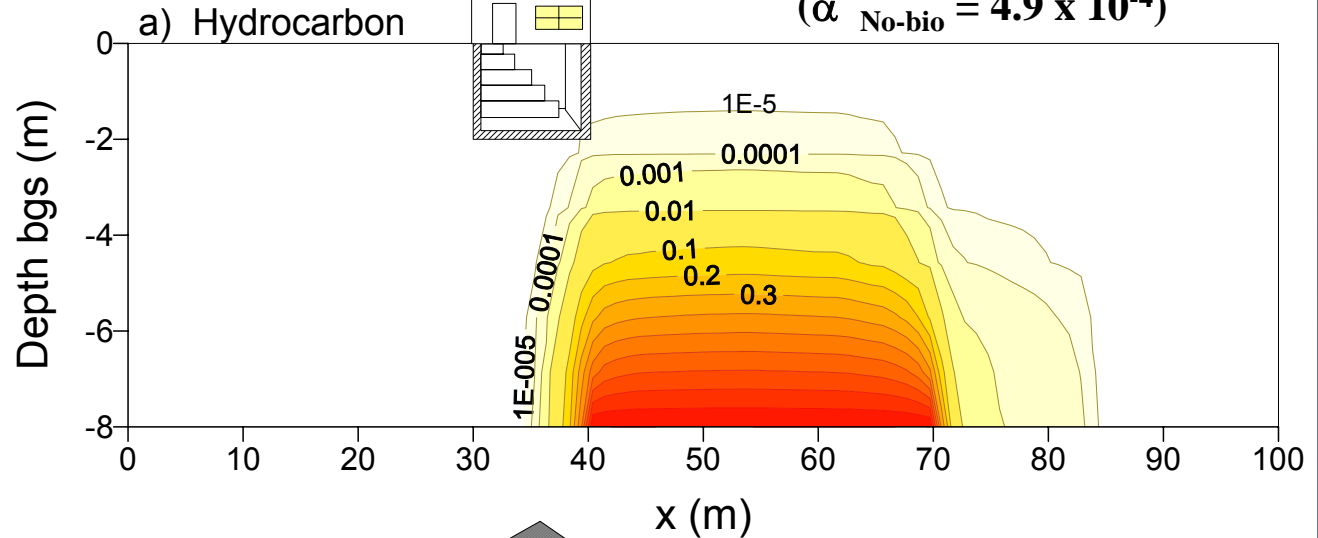
[Biodegradation,  
Basement Scenarios,  
 $C_{\text{source}} = 200 \text{ mg/L}$ ]

$$\lambda = 0.18 \text{ h}^{-1}$$

$$Q_s = 4.05 \text{ L/min}$$

$$\alpha_{\text{bio}} = 6.5 \times 10^{-9}$$

$$(\alpha_{\text{No-bio}} = 4.9 \times 10^{-4})$$



# Changes in $\alpha$ with Source Position

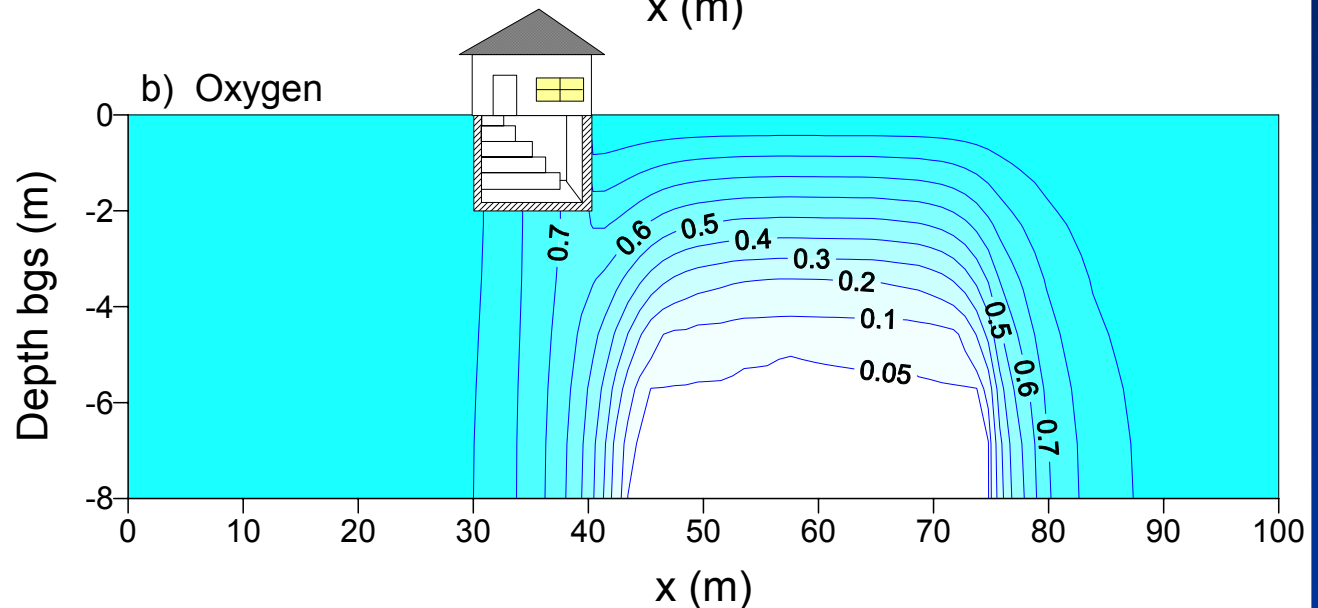
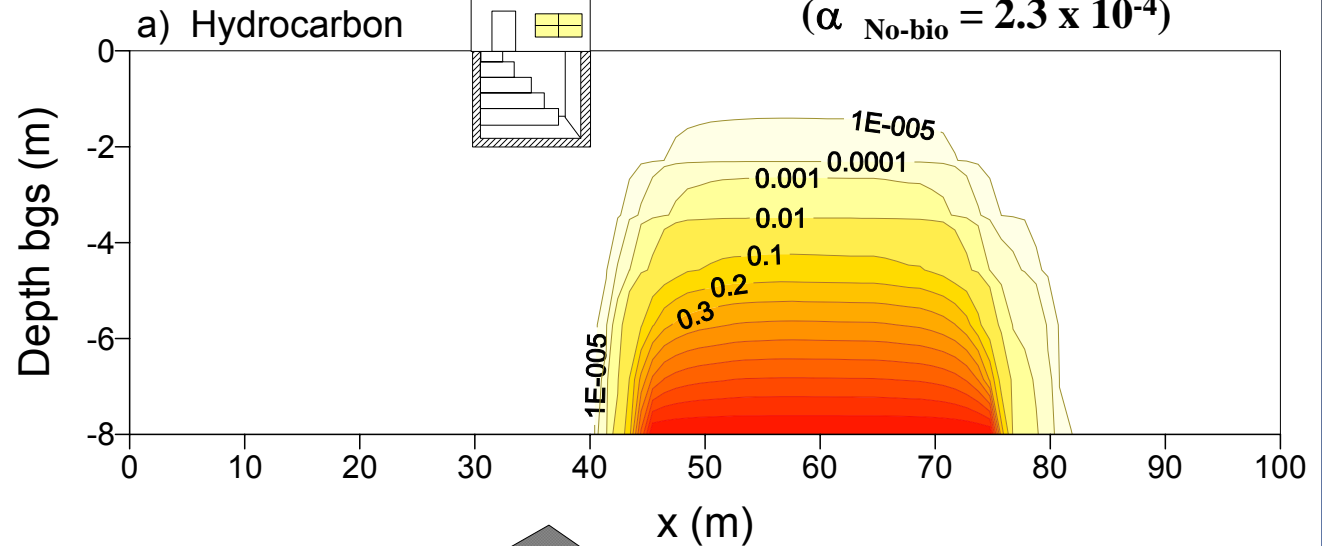
[Biodegradation,  
Basement Scenarios,  
 $C_{\text{source}} = 200 \text{ mg/L}$ ]

$$\lambda = 0.18 \text{ h}^{-1}$$

$$Q_s = 4.05 \text{ L/min}$$

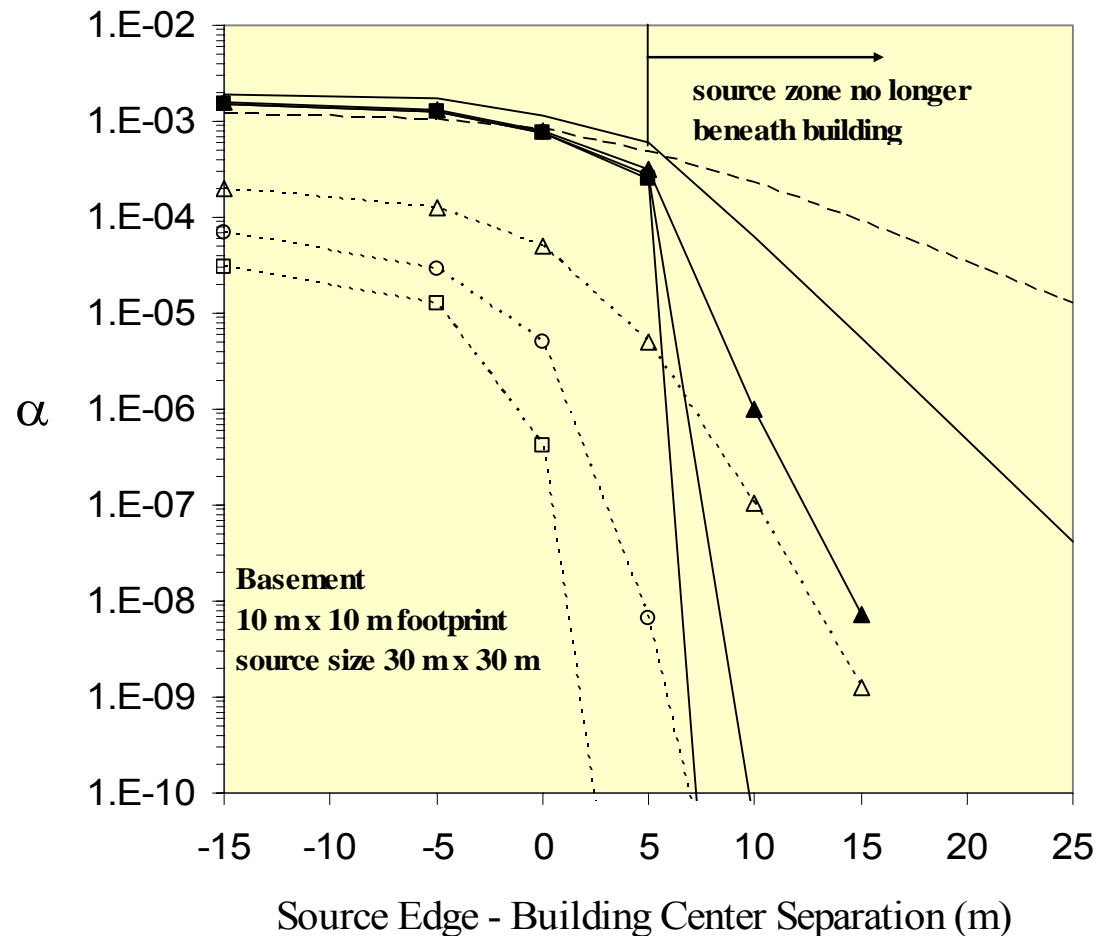
$$\alpha_{\text{bio}} = 1.1 \times 10^{-13}$$

$$(\alpha_{\text{No-bio}} = 2.3 \times 10^{-4})$$



# Changes in $\alpha$ with Source Position

Basement Scenarios,  
 $C_{\text{source}} = 200 \text{ mg/L}$ ,  
Depth = 3 and 8 m bgs



- |   |  |
|---|--|
| — 3 m bgs - No reactions                      | ---- 8m bgs - No reactions                       |
| —▲— 3 m bgs , $\lambda = 0.018 \text{ (1/h)}$ | ---△--- 8m bgs , $\lambda = 0.018 \text{ (1/h)}$ |
| —●— 3 m bgs , $\lambda = 0.18 \text{ (1/h)}$  | ---○--- 8m bgs , $\lambda = 0.18 \text{ (1/h)}$  |
| —■— 3 m bgs , $\lambda = 1.8 \text{ (1/h)}$   | ---□--- 8m bgs , $\lambda = 1.8 \text{ (1/h)}$   |

# Lessons-Learned for Scenarios with Aerobically-degradable Chemicals

- Vapor source concentration

While biodegradation may be significant over a wide range of concentrations, the effect of biodegradation on  $\alpha$  is more substantial for moderate to low source concentrations

- Vapor source depth

Biodegradation effects are more pronounced for larger source-foundation distances

- Lateral distance from buildings

Small source-building lateral separation (e.g., 5 - 10 m) can result in a very large reduction in  $\alpha$



# Lessons-Learned for Scenarios with Aerobically-degradable Chemicals

- Biodegradation rates

Range of biodegradation rates considered - high degradation rates affects  $\alpha$  more significantly than low degradation rates

- Crack location

Model predicted  $\alpha$  is not dependent on crack location for cases where biodegradation is significant and oxygen penetrates fully into the subsurface beneath the slab (i.e., low source concentration or deep sources)

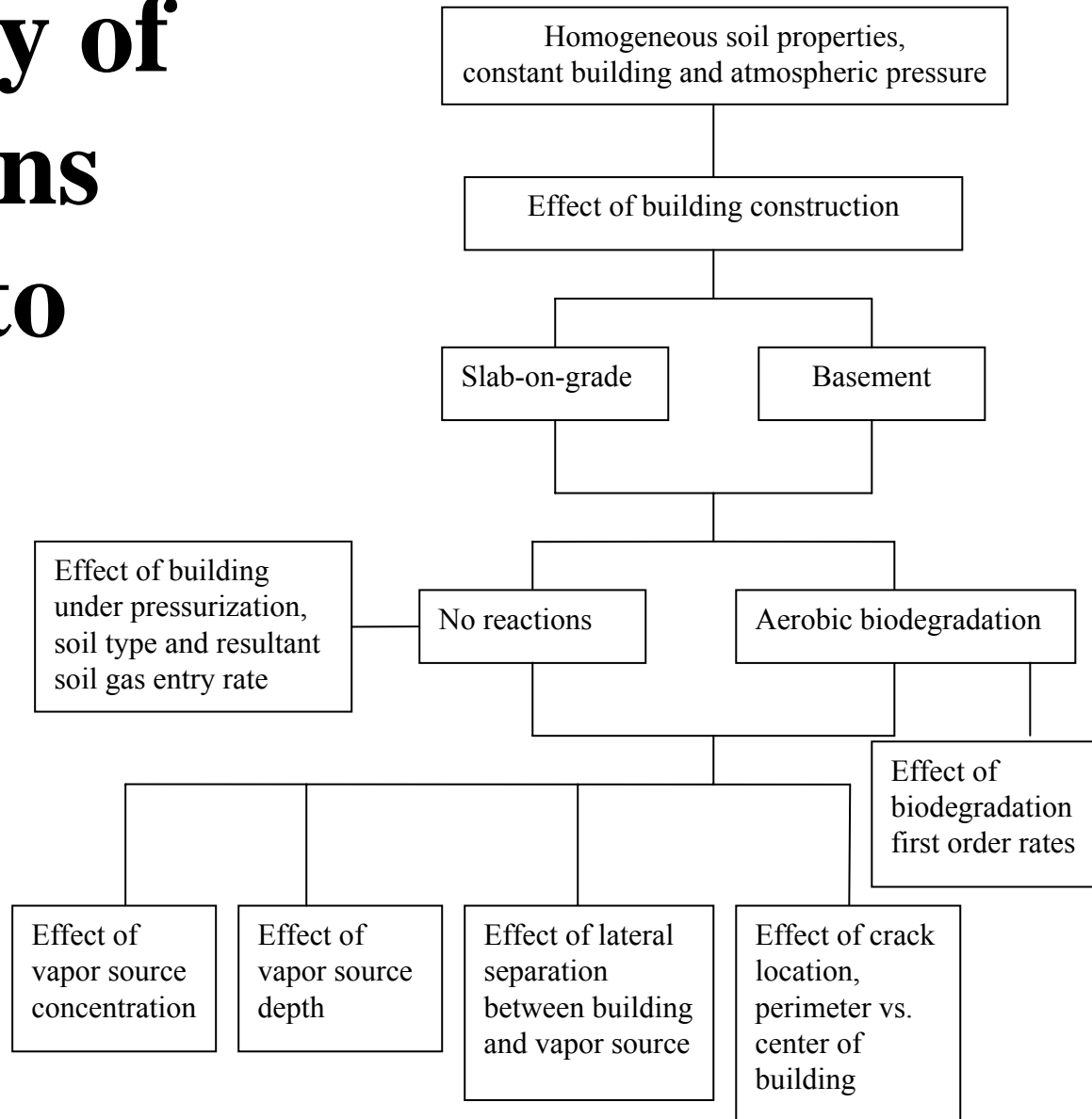
- Building construction

Slab-on-grade scenarios are more influenced by biodegradation than basement foundation scenarios



# Summary of Conditions Studied to Date

(Abreu 2005)





# Future Scenarios

- Layered lithology
- Wind blowing against the building
- Backfill and gravel layer around building foundation



# References

1. Abreu, L.D.V. 2005. A Transient Three-Dimensional Numerical Model to Simulate Vapor Intrusion Into Buildings. Ph.D. Dissertation. Arizona State University.
2. Abreu, L.D.V. and P.C. Johnson, 2005. Effect of Vapor Source-Building Separation and Building Construction on Soil Vapor Intrusion as Studied with a Three-Dimensional Numerical Model. *Environmental Science and Technology* 39(12), 4550-4561.
3. Abreu, L.D.V. and P.C. Johnson, 2005. Modeling the effect of aerobic biodegradation on soil vapor intrusion into buildings - Influence of degradation rate, source concentration, and depth. Submitted to *Environmental Science and Technology* (July 2005).



# Questions/Comments?

